Cyclic loading of suction caisson foundations for offshore wind turbines

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Offshore wind power

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Offshore wind turbines in the UK

- Government renewable energy policy

10% of electricity by 2010 from clean energy (6·10³MW)

32 turbines currently working (64MW)

- Why suction caisson foundations? (for 5MW turbines)

Gravity bases become very large in size and in weight

Piles require expensive equipment and long time for installation

Motivation



http://www.bwea.com/media/images/NorthHoyle©AnthonyUpton2003.jpg



Proposed monopod suction caisson foundation

3DOF rig



Loads and displacements in the reference point



Description of the tests carried out

- Two models of suction caissons:

1) *2R* = 293mm, *L* = 150mm, *t* = 3.4mm (*L/2R* = 0.5)

2) *2R* = 202mm, *L* = 200mm, *t* = 3.4mm (*L/2R* = 1)

- Dry and loose white Leighton Buzzard sand:

1) $Rd = 26\% \pm 13\% (L/2R = 0.5)$

2) $Rd = 20\% \pm 3\% (L/2R = 1)$

- Constant V, from -50N to 400N
- Constant ratio *M/2RH,* from -0.1 to 2
- 10 cycles at a velocity $2Rd\theta/dt = 0.02$ m/s

Results

2R = 293mm and V = 50N



-Hysteretic response -Masing rule Masing rule:

- the shape of the unloading and reloading curves is the same as that of the doubled initial curve
- ii) the tangent slope of the reloading curves is identical to the tangent slope of the initial curve

Proof of the Masing rule



Uplift and settlement occurring during cycling



√= 50N

V= 200N

Peaks of moment load – rotational displacement backbone curve



Peaks of load versus displacement: M/2RH = 1 and L/2R = 0.5



Conclusions

- Beneficial effect in the cyclic response of the caisson when the vertical load increases
- Evidence of uplift if the suction caisson is in a condition of V < M/2R or V < H (for L/2R = 0.5)
- Secant stiffness reduces with the amplitude of cycle
- Proof of the Masing rules
- Results to be used in the construction of a continuous hyperplasticity model